

# Anisotropic adaptivity for the finite element solutions of three-dimensional convection-dominated problems

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## SUMMARY

Convection-dominated problems are typified by the presence of strongly directional features such as shock waves or boundary layers. Resolution of numerical solutions using an isotropic mesh can lead to unnecessary refinement in directions parallel to such features. This is particularly important in three dimensions where the grid size increases rapidly during conventional isotropic refinement procedures. In this work, we investigate the use of adaptive finite element methods using anisotropic mesh refinement strategies for convection-dominated problems. The strategies considered here aim to resolve directional features without excessive resolution in other directions, and hence achieve accurate solutions more efficiently. Two such strategies are described here: the first based on minimization of the least-squares residual; the second based on minimizing a finite element error estimate. These are incorporated into an *hr*-adaptive finite element method and tested on a simple model problem. Copyright © 2002 John Wiley & Sons, Ltd.

KEY WORDS: anisotropic adaptivity; finite element; convection dominated

## 1. INTRODUCTION

In this work we investigate the use of anisotropic mesh refinement algorithms for the adaptive finite element (FE) solution of three-dimensional convection-dominated flow problems. Conventional mesh adaptivity, based upon *a posteriori* error estimation and regular *h*-refinement for example, is not always efficient for this class of problem; where solutions often exhibit strongly directional features such as sharp layers or shocks. In these regions of the solution isotropic mesh refinement results in an unnecessary level of resolution parallel to the flow feature being captured in order to deliver the required resolution across the feature. In many such situations an appropriate anisotropic mesh can yield an equivalent accuracy using substantially

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fewer degrees of freedom, and therefore at a potentially significantly reduced computational cost.

The fundamental issue that is considered in this paper is that of how to automatically adapt a three-dimensional tetrahedral mesh in order to obtain appropriate anisotropic meshes for convection-dominated problems. Our approach is to combine a standard local  $h$ -refinement algorithm [1], with the use of local node movement in order to either drive down a norm of the residual [2], or a local *a posteriori* error estimate [3]. Details of these techniques are provided in the following two sections. Following this, in Section 4, we present a modification of the node movement algorithm which permits nodes at different levels of the mesh hierarchy to be moved independently. An example is presented which demonstrates the advantage of being able to move the nodes on the coarsest mesh only, dragging higher level nodes with them. The paper concludes with a brief discussion of how we are currently developing this work to permit the solution of time-dependent equations and systems.

## 2. LEAST-SQUARES RESIDUAL MINIMIZATION

Here we present a three-dimensional generalization of previous work in two dimensions, [4, 2, 5], which aims to combine node movement (frequently referred to as  $r$ -refinement) with local  $h$ -refinement in order to drive down a given functional (which is bounded below). For simplicity we describe the application of our technique to a simple linear hyperbolic model problem of the form

$$(\mathbf{a} \cdot \nabla)u = f \quad \text{in } \Omega = (0, 1)^3 \quad (1)$$

$$u = \begin{cases} 1 - x/\delta & x < \delta \\ 0 & x \geq \delta \end{cases} \quad \text{on } \Gamma_{in} = \{\mathbf{x} \in \partial\Omega : \mathbf{a} \cdot \mathbf{n}(\mathbf{x}) < 0\} \quad (2)$$

where  $\mathbf{n}(\mathbf{x})$  is the unit outward normal to the boundary  $\partial\Omega$ . Figure 1 illustrates the nature of the solution of this problem when  $f(\mathbf{x}) = 0$ ,  $\mathbf{a} = (2, 1, 1)^T$  and  $0 < \delta \ll 1$ . The figure shows the isosurface  $u(\mathbf{x}) = 0.5$  and the solution changes rapidly from 0 to 1 as one moves across this

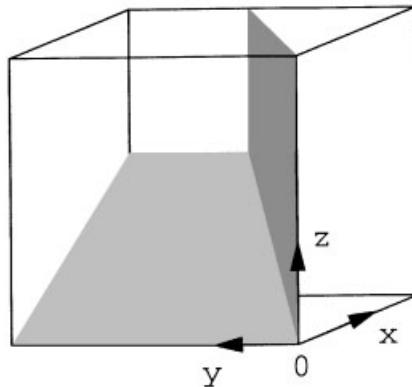


Figure 1. The strongly directional layer that is present in the solution of the model problem.

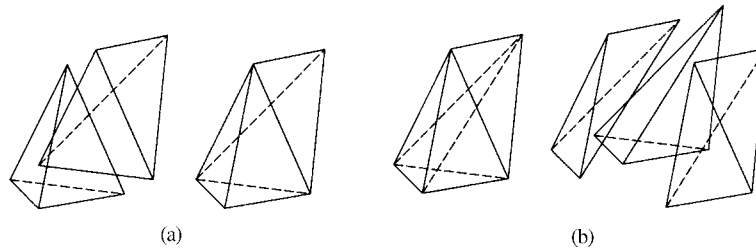


Figure 2. Local reconnection operation for the union of 2 tetrahedra: (a) two initial tetrahedra; (b) three modified tetrahedra.

isosurface. In all of the calculations which follow we use  $\delta = 0.01$  and the above choices of  $f(\mathbf{x})$  and  $\mathbf{a}$ .

In order to define a suitable functional for minimization we consider the residual of (1) for a piecewise linear approximation to  $u, u^h$  say, on a tetrahedral mesh which covers  $\Omega$

$$r^h = f - (\mathbf{a} \cdot \nabla)u^h \quad (3)$$

Following Reference [2] we now introduce the functional

$$R(u^h) = \frac{1}{2} \int_{\Omega} (r^h)^2 \, d\mathbf{x} = \frac{1}{2} \sum_k \int_{\Omega^k} (r^h)^2 \, d\mathbf{x} \quad (4)$$

where the summation is over all tetrahedra  $\Omega^k$  in the given mesh. The optimization scheme that we apply is as follows:

1. Order the nodes of the mesh according to their distance downstream of the inflow boundary.
2. For each node  $i$  (located at  $\mathbf{x}_i$ , say) in this ordering:
  - (a) find  $\partial R / \partial \mathbf{x}$  (details of this calculation are given in Appendix A).
  - (b) perform a 1-D minimization of  $R$  in this direction of steepest descent.
  - (c) solve a local version of (1) on the elements surrounding node  $i$  to update the solution values at this node and those on the downstream boundary of this patch.
 Repeat this step a fixed number of times.
3. For each internal face in the mesh consider reconnecting the union of the two tetrahedra sharing this face into three tetrahedra as shown in Figure 2; the topology yielding the lower value of (4) being accepted.
4. Perform  $h$ -refinement on those elements with a local  $L^2$  residual greater than a fixed fraction of the maximum residual and recompute the global least-squares solution.

The ordering of the nodes in step 1 is not essential, however, it dramatically improves the convergence of the minimization procedure in step 2 (for the computations presented here only 3 repetitions of this step are required, for example). The  $h$ -refinement in step 4 uses a fixed fraction strategy which allows a simple comparison to be made between  $h$  and  $hr$  algorithms, since similar numbers of elements will be produced after each refinement stage. Here the top 20% of the elements, ranked by their local  $L^2$  residual, are refined. The algorithm can be terminated when either a desired value of the least-squares residual is obtained or a

Table I. Sample results using the residual minimization scheme.

	<i>hr</i> -Refinement			<i>h</i> -Refinement		
	$N_p$	$R(u^h)$	$\ e\ _1$	$N_p$	$R(u^h)$	$\ e\ _1$
Solve	729	1.016	0.075	729	1.016	0.075
Optimize		0.381	0.056			
Adapt/solve	3072	0.189	0.034	3313	0.428	0.180
Optimize		0.130	0.031			
Adapt/solve				15 353	0.180	0.031

maximum number of elements has been reached. The need for the simple ‘edge-swapping’ sweep (step 3) is illustrated in 2-D in References [4, 2, 6] for example. This assists with the alignment of the edges in the mesh with the flow features that we wish to capture.

Table I illustrates some sample results obtained when the proposed scheme is applied to our linear model problem. It is apparent that, measured either in terms of the residual or the exact error, the *hr*-refinement approach provides a significant improvement over the use of local *h*-refinement alone (in this calculation a similar accuracy is obtained with just a fifth of the number of node points ( $N_p$ ) for example).

### 3. MINIMIZATION OF ESTIMATED *a posteriori* ERROR

As an alternative to controlling the mesh adaptivity process through the local residual we now consider the use of an *a posteriori* error estimate. Provided that the error can be estimated sufficiently accurately it is clearly more desirable to control this quantity. Our approach is the commonly used one of References [7, 3], for example, where it is observed that subtraction of (1) from (3) yields the error equation

$$(\mathbf{a} \cdot \nabla)e = r^h \quad (5)$$

for  $e = u - u^h$ . This PDE is solved subject to an exact inflow boundary condition on  $\Gamma_{in}$  but using either a different mesh or numerical scheme from that applied to obtain  $u^h$ . In this work we use a stable streamline-diffusion linear finite element method [8], to calculate  $u^h$  and a cell-centred finite volume scheme [9], to compute  $e^h$  (an estimate of  $e$ ) on each element. The adaptivity algorithm that we then apply is as follows:

1. For each node in the mesh:
  - (a) find

$$\mathbf{x}_i^{av} = \frac{\sum_{k \in \Omega_i} |e_k^h| \mathbf{x}_k^c}{\sum_{k \in \Omega_i} |e_k^h|}$$

where  $\Omega_i = \{k : \mathbf{x}_i \in \overline{\Omega^k}\}$ ,  $e_k^h$  is the computed error in cell  $k$  and  $\mathbf{x}_k^c$  is the position of the centroid of cell  $k$ ,

- (b) set  $\mathbf{x}_i := (1 - \gamma)\mathbf{x}_i + \gamma\mathbf{x}_i^{av}$ , where  $\gamma \in (0, 1)$  is an under-relaxation parameter, taken here to be fixed at  $\gamma = 0.5$ .

Table II. Sample results using  $r$ -refinement driven by the error.

$hr$ -Refinement				$h$ -Refinement			
Driven by $e$		Driven by $e^h$		Driven by $e$		Driven by $e^h$	
$N_P$	$\ e\ _1$	$N_P$	$\ e\ _1$	$N_P$	$\ e\ _1$	$N_P$	$\ e\ _1$
729	0.111	729	0.111	729	0.111	729	0.111
	0.104		0.104				
	0.094		0.102				
2826	0.052	3021	0.069	2761	0.070	2799	0.079
	0.050		0.065				
	0.046		0.062				
12 412	0.038	12 260	0.043	12 026	0.045	11 437	0.051
	0.033		0.039				
	0.029		0.037				
50 737	0.020	44 051	0.026	52 871	0.027	44 105	0.032
	0.018		0.023				
	0.016		0.022				

Repeat this step a fixed number of times.

2. Perform  $h$ -refinement on those elements with an estimated error greater than a fixed fraction of the maximum error on any element and recompute the global solution and error estimate.

Step 1 is repeated 3 times for the computations presented here, further repetitions do not lead to any significant increase in accuracy. The fixed fraction for  $h$ -refinement is again taken to be 20%. As in the previous section, these steps may be repeated until a desired value of the estimated error is obtained or a maximum number of elements has been reached. Note that, unlike for the residual minimization approach there is no straightforward mechanism for incorporating edge-swapping into this algorithm.

Table II presents some sample results when this algorithm is used to solve the linear model problem previously considered. In order to allow the dependency on our choice of solver for (5) to be assessed additional statistics are presented to show how the algorithm performs when the exact error, which is known for this problem, is used rather than the estimated error  $e^h$ . In both cases the  $hr$ -refinement scheme again outperforms standard  $h$ -refinement, with similar errors requiring about a third the number of node points. An indication of the contrasting meshes produced by these two forms of adaptivity is provided in Figure 3.

#### 4. HIERARCHICAL $r$ -REFINEMENT

It has been demonstrated that the inclusion of node movement within each of the adaptive algorithms considered leads to better quality meshes than are otherwise obtained. Furthermore, from Figure 3, it may be observed that this node movement allows the element shape to deform in line with the anisotropic features of the solution. It should be noted however that the cost of the node movement grows significantly as the size of the finite element

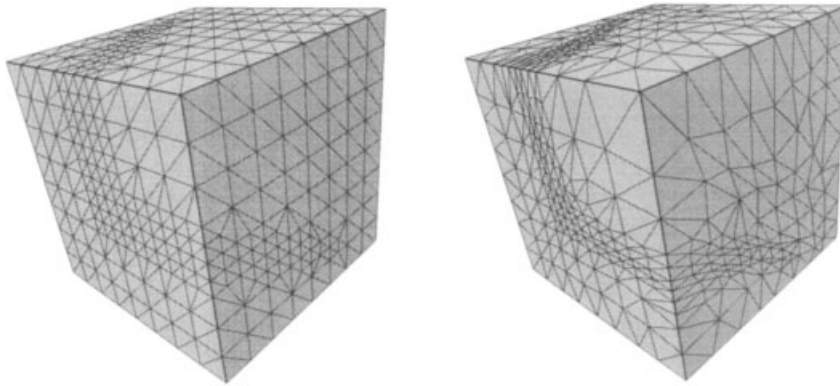


Figure 3. Two sample meshes obtained during the solution of the model problem: the first, obtained using  $h$ -refinement, contains 13 002 elements but leads to a solution error which is almost twice that of the second grid, containing 13 343 elements, obtained using  $hr$ -refinement.

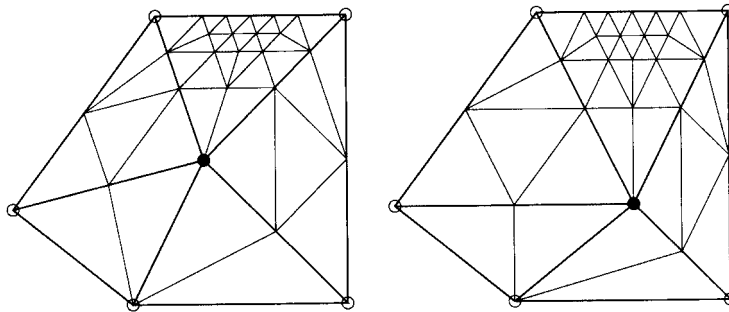


Figure 4. The movement of a root mesh node in two dimensions.

mesh increases since the position of every node must be updated independently at each  $r$ -refinement step. The main development that we consider in this section therefore is to utilize the  $h$ -refinement hierarchy in order to move only the coarse mesh nodes independently, with the movement of the nodes produced at finer mesh levels being dependent upon this.

The proposed approach is to follow essentially the same algorithms as outlined in the previous sections but, instead of looping through every node in the mesh at the  $r$ -refinement stage, only the nodes contained in the initial mesh (i.e. the root mesh, at the lowest level of the  $h$ -refinement hierarchy) are visited. When the position of one of these nodes is updated then so too is the position of all nodes in the interior of the patch of root mesh elements surrounding this node. This is illustrated for a two-dimensional example in Figure 4. Note that the dependent node positions are updated so that their barycentric co-ordinates with respect to the root mesh elements remain unchanged.

For clarity we describe the detail of this approach in the context of the residual minimization procedure of Section 2. In particular, we note that the ‘edge-swapping’ phase may still be

Table III. An example where the root node movement strategy proves to be advantageous over the original version of the algorithm in which all node positions are updated independently.

	Original <i>hr</i> -refinement			Modified <i>hr</i> -refinement		
	$N_p$	$R(u^h)$	$\ e\ _1$	$N_p$	$R(u^h)$	$\ e\ _1$
Global solve	4913	53.45	0.0237	4913	53.45	0.0237
<i>r</i> -Refine/local solve		13.78	0.0059		7.39	0.0028
<i>h</i> -Refine/global solve	13 536	4.05	0.0016	13 155	2.05	0.0007
<i>r</i> -Refine/local solve		2.57	0.0010		1.88	0.0007
<i>h</i> -Refine/global solve	40 186	1.47	0.0004	38 606	0.54	0.0002
<i>r</i> -Refine/local solve		1.33	0.0004		0.54	0.0002

completed in principle although it does add significantly to the overall complexity of the implementation. The calculation of  $\partial R/\partial \mathbf{x}_i$ , at step 2(a) is also made more expensive since

$$\frac{\partial R}{\partial \mathbf{x}_i} = \sum_{j \in \mathcal{P}_i} \theta_{i,j} \frac{\partial R}{\partial \mathbf{x}_j} \quad (6)$$

where  $\mathcal{P}_i = \{j: \mathbf{x}_j \in \{\text{points in those root mesh elements with a vertex at } \mathbf{x}_i\}\}$  and  $\theta_{i,j}$  is the barycentric co-ordinate of  $\mathbf{x}_j$  with respect to the vertex of its parent root element that is  $\mathbf{x}_i$ . It should be noted however that all expressions (6), i.e. for each root node  $i$ , may be assembled together in a single loop through the leaf mesh elements (making use of expression (10) in Appendix A). Table III presents a comparison of using this root node movement approach with the original *hr*-refinement algorithm for a slightly different test problem to (1) which has the solution  $u(\mathbf{x}) = e^{-x_1/\delta}$ . When  $\delta$  is small (0.01 in this example) this solution has a boundary layer next to  $x_1 = 0$ . It is apparent that, for this particular problem, coarse mesh movement is advantageous since it allows the nodes to move into the boundary layer region near  $x_1 = 0$  more quickly than with the original *r*-refinement approach.

## 5. DISCUSSION

The generalization of both the least-squares solution technique and the *a posteriori* error estimate to linear systems of equations is relatively straightforward and hence the adaptive algorithms introduced in this paper may both be applied to such problems. Clearly, if different components of the solution have different directional behaviour then the scope for using anisotropic meshes will be reduced, however for many physical problems similar directional solution features are present in all components and the benefits of our *hr*-refinement strategies will again become apparent. Extensions to time-dependent problems are also under development with the aid of the hierarchical *r*-refinement described in Section 4. By only moving the root mesh nodes independently it is still possible to apply both *h*-refinement and derefinement (necessary for time-dependent problems [1]) without disturbing the mesh hierarchy within the adaptive *h*-refinement code.

## APPENDIX A: NODAL DERIVATIVES OF THE RESIDUAL FUNCTIONAL

In order to determine the direction of steepest decent in the residual minimization algorithm of Section 2 it is necessary to evaluate expressions of the form  $\partial R/\partial \mathbf{x}_i$ , where  $\mathbf{x}_i$  is the location of node  $i$ . In order to do this we use the following two results which are proved in References [10, Theorem 2.4, 11, Lemma 3.1], respectively

$$\frac{\partial u^h}{\partial \mathbf{x}_i} = -N_i \nabla u^h \quad (\text{A.1})$$

$$\frac{\partial V^k}{\partial \mathbf{x}_i} = V^k \nabla N_i \quad (\text{A.2})$$

Here  $V^k$  is the volume of any simplex  $\Omega^k$  which has a vertex at  $\mathbf{x}_i$ , and  $N_i$  is the usual piecewise linear basis function which has value 1 at  $\mathbf{x}_i$ . From (3) and (4) we have

$$\begin{aligned} \frac{\partial R}{\partial \mathbf{x}_i} &= \frac{1}{2} \sum_{k \in \Omega_i} \frac{\partial}{\partial \mathbf{x}_i} \int_{\Omega^k} (f - (\mathbf{a} \cdot \nabla) u^h)^2 \, d\mathbf{x} \quad (\text{where } \Omega_i = \{k : \mathbf{x}_i \in \overline{\Omega^k}\}) \\ &= \frac{1}{2} \sum_{k \in \Omega_i} \frac{\partial}{\partial \mathbf{x}_i} \int_{\Delta} (f - (\mathbf{a} \cdot \nabla) u^h)^2 V^k \, d\xi \\ &\quad (\text{where } \Delta \text{ is some reference tetrahedron with unit volume}) \\ &= \sum_{k \in \Omega_i} \int_{\Delta} \left[ (f - (\mathbf{a} \cdot \nabla) u^h) \left( -(\mathbf{a} \cdot \nabla) \frac{\partial u^h}{\partial \mathbf{x}_i} \right) V^k + \frac{1}{2} (f - (\mathbf{a} \cdot \nabla) u^h)^2 \frac{\partial V^k}{\partial \mathbf{x}_i} \right] d\xi \\ &= \sum_{k \in \Omega_i} \int_{\Omega^k} \left[ (f - (\mathbf{a} \cdot \nabla) u^h) ((\mathbf{a} \cdot \nabla) N_i) \nabla u^h + \frac{1}{2} (f - (\mathbf{a} \cdot \nabla) u^h)^2 \nabla N_i \right] d\mathbf{x} \\ &\quad (\text{where (A.1) and (A.2) have been applied}) \end{aligned} \quad (\text{A.3})$$

Hence, when  $f(\mathbf{x})=0$ , as in our example problem, expression (A.3) simplifies further to yield

$$\frac{\partial R}{\partial \mathbf{x}_i} = \sum_{k \in \Omega_i} V^k ((\mathbf{a} \cdot \nabla) u^h)_k \left( \frac{1}{2} ((\mathbf{a} \cdot \nabla) u^h)_k \nabla N_i - ((\mathbf{a} \cdot \nabla) N_i)_k \nabla u^h \right) \quad (\text{A.4})$$

where  $(\cdot)_k$  denotes the restriction of the quantity within the brackets to element  $k$ .

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